

HIGH-FREQUENCY MODELS OF THE BJT

- The dominant model used for small-signal analysis of a BJT in the forward-active region, the h -parameter model as presented in Chapter 3, does not contain frequency sensitive elements and is therefore invariant with respect to changes in frequency. It is therefore necessary to introduce a new BJT model or to reinterpret an old model to include frequency-dependent terms using the Ebers-Moll model as a basis for creating the new model.
- In the forward-active region and at low frequencies the Ebers-Moll Model can be replaced by the linear two-port model shown in Figure 10.4-2. This model is known as the hybrid- π model. It is similar to the h -parameter model used previously in this text, but has particular utility when frequency-dependent terms are included.

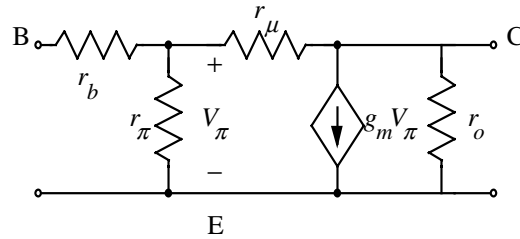


Figure 10.4-2 Low-frequency Hybrid- π BJT Model

- The relationships between h -parameter and hybrid- π models are related to the h -parameter model parameters by:

$$g_m = \frac{h_{fe}}{r_\pi} = \frac{|I_c|}{\eta V_t}, \quad r_\pi = \beta_F \frac{\eta V_t}{|I_c|} = \frac{\beta_F}{g_m},$$

$$r_o \approx \frac{1}{h_{oe}} = \frac{|V_A|}{|I_c|}, \quad r_b = h_{ie} - r_\pi.$$
- As will be seen in Section 10.7, the hybrid- π model is also useful in modeling FETs.
- The frequency-dependent component of transistor behavior is based on the capacitive component of p-n junction impedance. Once the capacitive nature of a p-n junction is known, a frequency dependent model for a BJT can be obtained.

Modeling a p-n Junction Diode at High Frequencies

- The charge buildup in the semiconductor region near a p-n junction under a voltage bias, causes a significant buildup of electrical charge on each side of the junction which exhibits acts as a capacitance. It is modeled as a capacitor shunting the dynamic resistance of the junction (Figure 10.4-3).

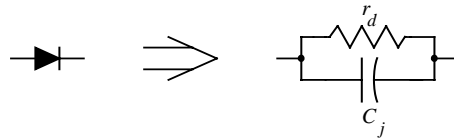


Figure 10.4-3 High-frequency model of a p-n junction

- In most electronic applications the p-n junction capacitance is dominated by the diffusion of carriers in the depletion regions. A good analytic approximation of this depletion

capacitance, C_j , is given by:
$$C_j \approx \frac{C_{jo}}{(1 - V_d)^m}, \quad (10.4-2)$$

where,

- C_{jo} = small-signal junction capacitance at zero voltage bias,
- ψ_o = junction built-in potential, and
- m = junction grading coefficient ($0.2 < m \leq 0.5$).

- A plot the junction capacitance as described by Equation 10.4-2 is shown in Figure 10.4-4.

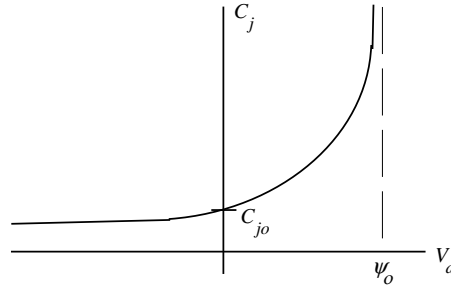
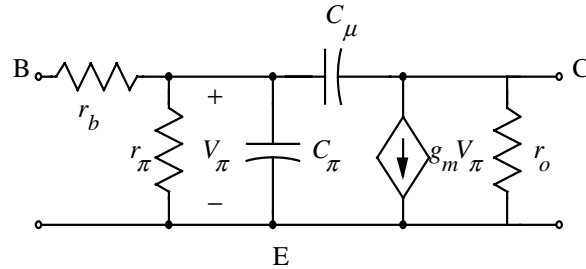


Figure 10.4-4 p-n Junction Depletion Capacitance

Modeling the BJT at High Frequencies in the Forward-Active Region

- In order to model the BJT at high frequencies, the hybrid- π model of Figure 10.4-2 is altered by shunting each p-n junction dynamic resistance with an appropriate junction capacitance.

Figure 10.4-5 The High-Frequency Hybrid- π Model of a BJT

- The junction capacitance, C_{μ} , is *relatively* independent of quiescent conditions. Typical manufacturer data sheets provide a value for C_{μ} at a given reverse bias (typically, $V_{CB} = 5$ or 10 V).
- The forward-biased base-emitter junction exhibits greater variation with bias conditions: its junction capacitance, C_{π} , must therefore be determined with greater caution.
- In order to correlate these measurements with the hybrid- π parameters, an ac equivalent circuit of the test circuit must be created (Figure 10.4-7).
- The gain-bandwidth product: the product of short-circuit current gain,

$$A_i(\omega) = (g_m) \left(\frac{r_{\pi}}{1 + j\omega r_{\pi}(C_{\pi} + C_{\mu})} \right) = \frac{h_{fe}}{1 + j\omega r_{\pi}(C_{\pi} + C_{\mu})} \text{ at a particular frequency and that}$$

frequency has constant value for all frequencies greater than $\omega_{3dB} = \frac{1}{r_{\pi}(C_{\pi} + C_{\mu})}$ is a common

$$\text{description: } \omega_T = \frac{h_{fe} - 1}{r_{\pi}(C_{\pi} + C_{\mu})} \approx \frac{g_m}{C_{\pi} + C_{\mu}} \quad (10.4-6)$$

- Manufacturers data sheets will either provide a value for ω_T or provide the gain at some other high frequency. The gain-bandwidth is given by: $\omega_T = A_m \omega_m$ (10.4-7)
where ω_m is the frequency at which the manufacturer made the gain measurement and A_m is the gain at that frequency.